Perceptual Spatial Audio Simulation and Reproduction

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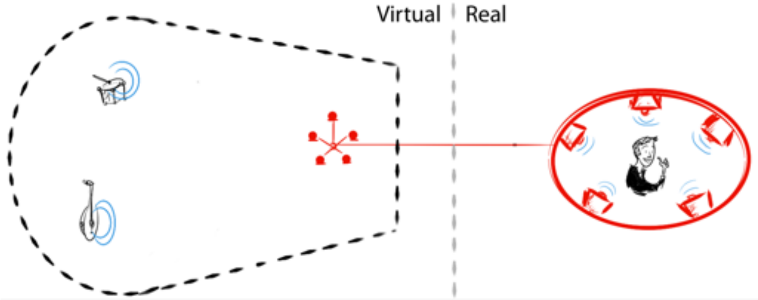
Objective

- Making listener feel transported to a different auditory scene
- This talk focuses on virtual scene, but same concepts can be applied to real (recorded) scene
- Applications in video games, VR/AR, architectural acoustics..



Outline

Acknowledgements

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Prof Zoran Cvetkovìc (King's College London)
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Prof Marc Moonen (KU Leuven)
Dr Niccoló Antonello (KU Leuven)
Stojan Djordjevic (University of Surrey)
Ashley Andrew-Jones (University of Surrey)
Ege Erdem (METU)

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About this talk

- Interrupt me!
- Details and maths left to references (at the end)
- Demos after this talk

Outline

Reproduction of plane waves

- Let's start from a relatively simple problem
- We want to reproduce a plane wave, and we assume that incident direction, θ_s, is known
- Relevant case for spatial audio objects (MPEG-H)
- The plane wave could represent e.g. a single sound source or a wall reflection
- If we solve this, summation of plane waves trivial (linearity)

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Reproduced plane wave should be:

1. perceived in correct direction (low localization error)
2. easy to localize (low localization uncertainty)

- in the largest possible area (large sweet spot)

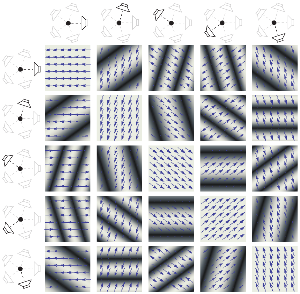
Physical and cross-talk cancellation methods

	SFR	Multichannel	2-Channel
Channel count	50+	< 10	2
Equipment Load	High	Commercially viable	Low
Psychoacoustics	None	Required	Critical
Sweet Spot	Large	Medium, small group	Small, individual

- Sound Field Reconstruction (SFR) provide mathematically elegant solution (e.g. HOA, WFS)...
  - but large number of loudspeakers: $r = \frac{c}{f}\frac{N}{2e\pi}$, e.g. $f = 10$ kHz, $r = 0.1$ m $\Rightarrow N = 56$
- 2-channel (cross-talk cancellation) methods, only two channels...
  - but small sweet spot (e.g. [Rose et al., 2002] report ≈ 3 cm)
- We'll focus on multichannel systems with limited equipment load, which need to leverage somehow psychoacoustics effects

How many loudspeakers to use to reproduce plane wave?

- **First question**: should we use > 2 loudspeakers for each source?
- Active intensity (AI) fields for plane waves



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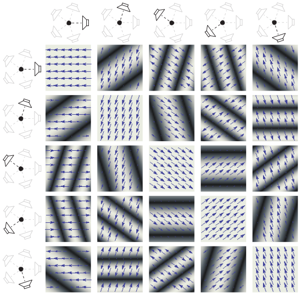
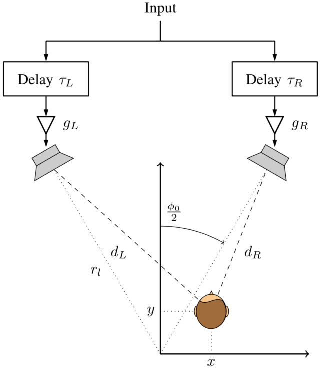


- Fluctuation speed depends on angle between loudspeaker pair
- **Answer**: use only the two loudspeakers closest to direction of plane wave [De Sena et al., 2013]
- This reduces problem to good ol' stereophonic reproduction

Frequency-independent inter-channel differences

- What should we do with these two loudspeakers?

- Consider frequency independent inter-channel time differences (ICTD) and level differences (ICLD)
- ICTD/ICLDs lead to low coloration [Spors et al., 2013], which is most important attribute for sound quality [Rumsey et al., 2005]



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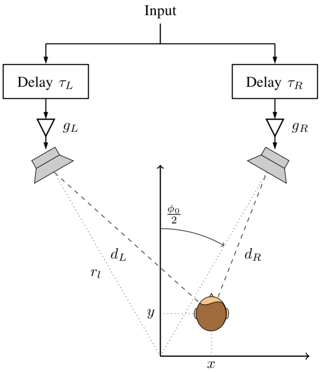
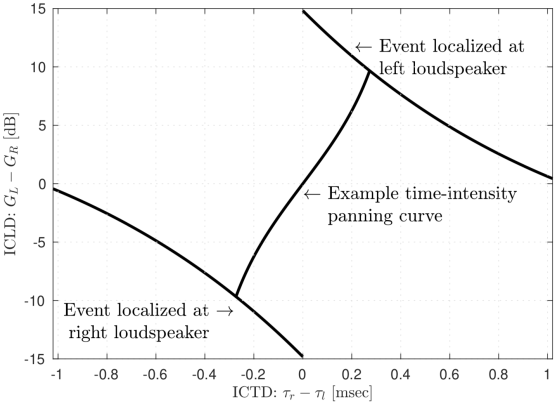


- As long as ICTD below echo threshold, listeners will perceive a fused "phantom source" (summing localization effect)

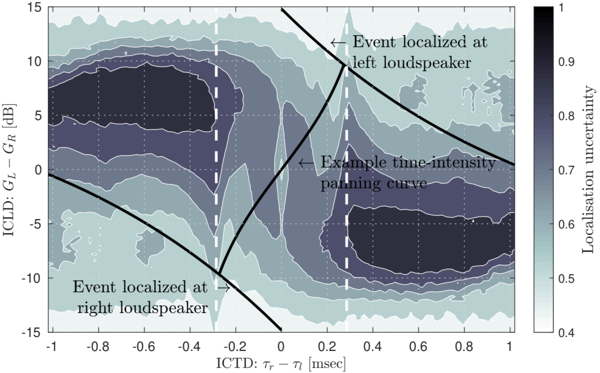
Position of phantom source

- Position of phantom source depends on ICTD/ICLD pair
- Same position can be achieved with different ICTD/ICLD pair
- One can use e.g. intensity only (most commercial sound recordings), time only, or time-intensity



Not all ICTD/ICLD pairs are created equal

- ICTD/ICLD pairs lead to different localization uncertainty
- Computational model in [De Sena et al., 2019]:



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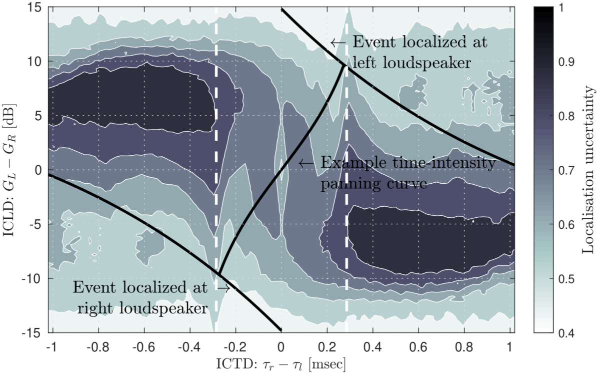
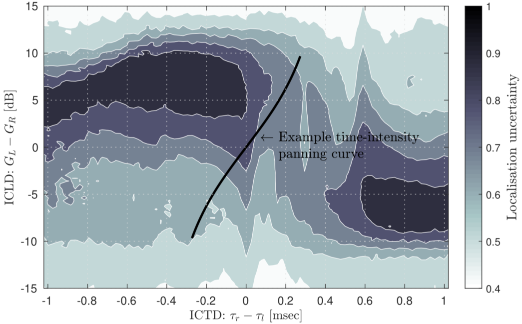


- Inconsistent ICTD/ICLD lead to high uncertainty
- Vertical bands: 2 replicates at one ear, but only 1 at other
- Intensity-only methods have lowest uncertainty

Localization uncertainty in off-center positions



- Listener moves 10 cm to the right, then entire plot moves (approximately) to the right
- Now intensity methods lie in area with high uncertainty!
- Time-intensity largely avoids this area

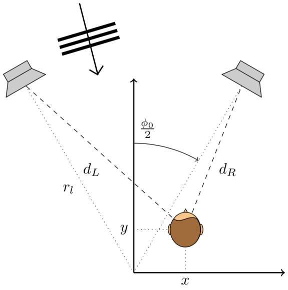
What is happening?

- Useful to define "relative" ICTD/ICLD as observed by the listener:

$$\mathrm{RICLD} \approx \mathrm{ICLD} - \frac{x}{r_l} \frac{20 \sin\left(\frac{\phi_0}{2}\right)}{\log_e(10)} ,$$

$$\mathrm{RICTD} \approx \mathrm{ICTD} - x \frac{2}{c} \sin\left(\frac{\phi_0}{2}\right) .$$

where ϕ_0 base angle, x lateral displacement and c speed of sound



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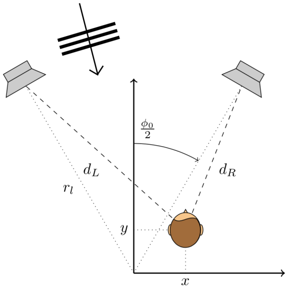
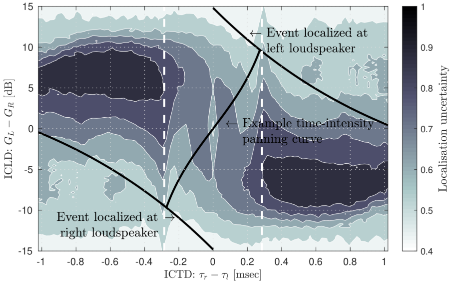


- E.g. consider ICTD = 0 ms and ICLD = 5 dB (left leading)
- RICTD = −0.29 and RICLD = 4.78, which are contradicting
- Adding a small ICTD will delay the onset of contradicting RICTD/RICLD pairs

Section Conclusions

- Intensity methods have lower uncertainty in center
- Time-intensity reduces uncertainty in off-center positions
- More ICTDs (within limits) $\Rightarrow$ lower uncertainty off-center
- Trade-off between uncertainty in center and off-center
- In general, unknown how much listener drifts from center
- We can e.g. set max ICTDs such that avoid vertical bands
- See [De Sena, 2019] for details of parametrization



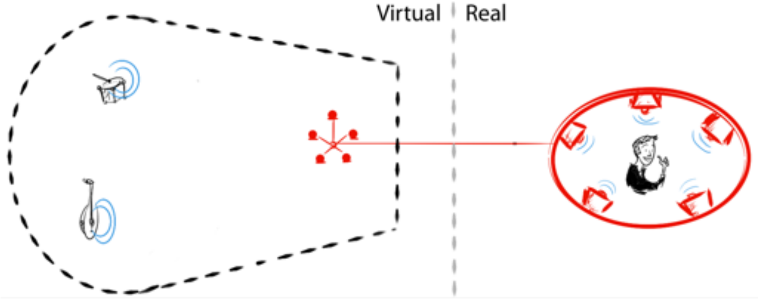
Extensions

- Concepts recently extended to third dimension [Erdem et al., 2019]
- Time-intensity in the vertical dimension leads to a perceived improvement in stability of sweet spot [Andrew-Jones, 2019]

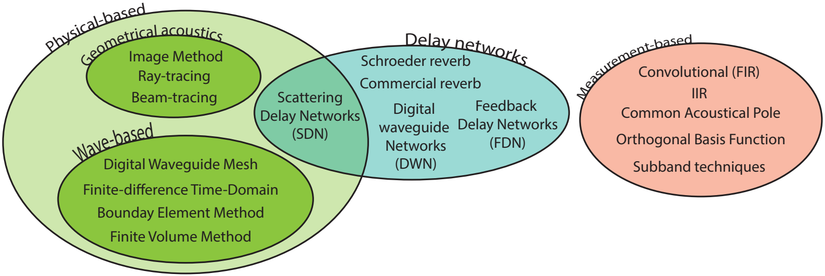
Outline

Perceptual Simulation of Room Acoustics

- So far we discussed how to render single plane waves, e.g. individual sound sources
- How do we simulate the acoustics of an entire space?



Overview



- Overview of more than 50 years of room acoustic simulation in [Välimäki *et al.*, 2012], [Välimäki *et al.*, 2016] and [Hacıhabiboğlu *et al.*, 2017]
- Wave-based models are the most accurate ones

Rendering of dynamic scenes with wave models

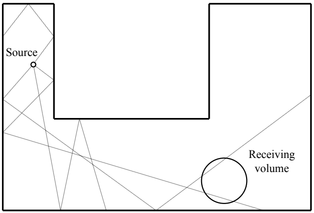
- In a complete wave model of a room:
  - sources and listeners can be moved
  - *spatialized* using microphone arrays or "virtual dummy head"

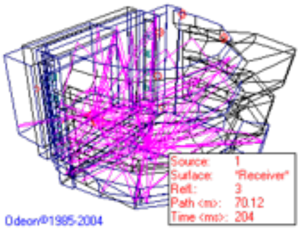
Example: How expensive is a wave-based model?

- Audio bandwidth $= 20$ kHz ≈ 1.27 cm wavelength
- Spatial samples every 0.63 cm or less
- $3.65 \times 5.8 \times 2.4$ m room requires > 200 million grid points
- 3D finite difference model requires one multiply and 6 additions per grid point $\Rightarrow$ 70 billion FLOPS at $F_s = 50$ kHz
- $30 \times 15 \times 6$ m concert hall requires $>$ *3 quadrillion FLOPS*

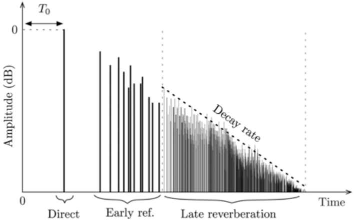
Geometric Models

- Geometric acoustics models have lower complexity
- Source emits rays in all directions
- Specular reflections (diffraction also possible)
- Build impulse response by recording time and amplitude at receiver
- Choice of receiver size and number of rays is critical





Room Impulse Response (RIR)



RIR components:

- Direct line-of-sight
- Early reflections: relatively sparse first echoes
- Late reverberation: so densely populated with echoes that it is best to characterise the response *statistically*.

Rendering of dynamic scenes with geometric models

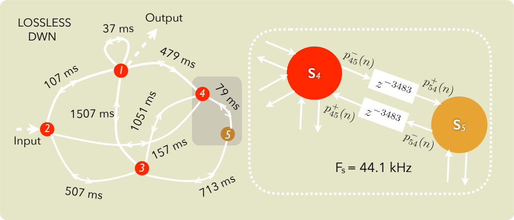
- When source moves recalculate RIR
- Still need to run a convolution with anechoic sound sample

Example:

- $T_{60} = 2$ s, $F_s = 50$ kHz: convolution requires 5 *billion* FLOPS
- Three sources and two listening points (ears) $\Rightarrow$ 60 billion FLOPS
- 20 dedicated CPUs clocked at 3 Gigahertz
- FFT convolution is faster, if throughput delay is tolerable (and there are low-latency algorithms)

- If physical accuracy not needed, perceptual methods provide better option

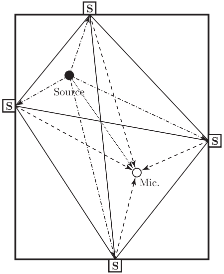
Digital waveguide networks (DWN)



- Network of bi-directional delay lines connected at scattering junctions [Smith, 1985]
- Can be interpreted as network of acoustic tubes
- **Question:** How to set parameters (delay line lengths, network connections, scattering matrix..)?

Scattering delay network (SDN) [De Sena et al., 2015]

- Design DWN based on characteristics of a physical room

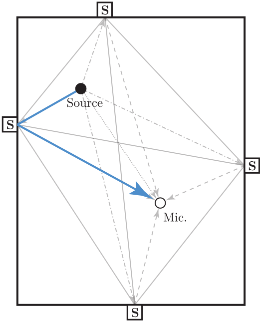


- Position nodes at first-order reflection points
- Fully connected DWN network
- Mono-directional lines for source-junction and junction-mic

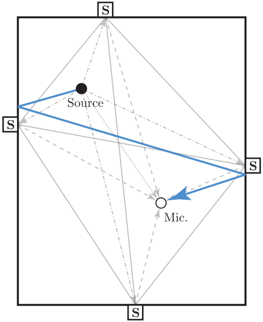
- Each incoming delay line on the microphone rendered as if it was a plane wave, using methods discussed in first part of talk

SDN: approximation of geometric acoustics

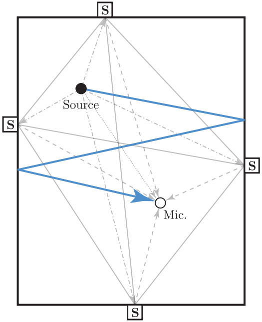
- Correct rendering of LOS and first-order reflections in time, amplitude and direction
- Approximation of second and higher-order reflections, less important perceptually



I-order reflection



II-order reflection



Another II-order reflection

SDN: approximation of geometric acoustics

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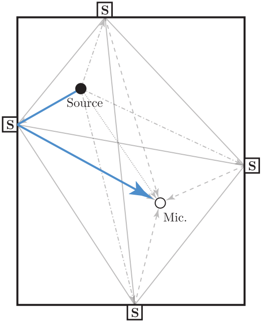

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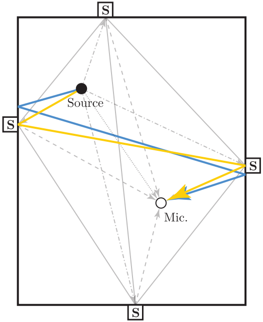
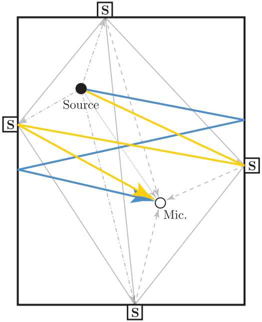


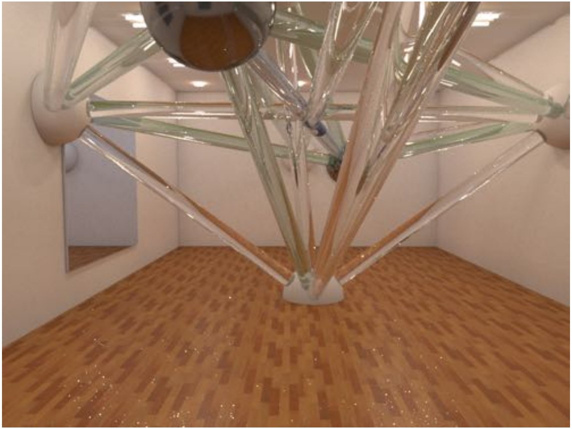
II-order reflection



Another II-order reflection

SDN: alternative interpretation

- Can also be interpreted as model of network of acoustic tubes



Advantages

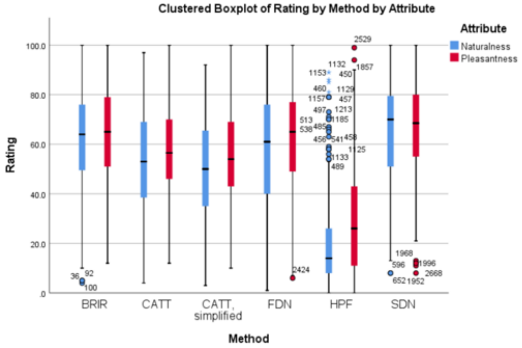
- Less resources spent for less important part of room impulse response (late reverberant tail)
- Also, not shown here:
  - similar frequency-dependent RT60 to full-scale models
  - similar echo density to full-scale models
  - sufficient modal density
  - axial resonant modes of room well approximated
- Orders of magnitude faster than convolution (alone!)
- All parameters of model derived from physical properties

Advantages w.r.t. other delay networks:

- No need for hands-on parameters tuning
- Physical interpretation $\Rightarrow$ spatialisation possible, e.g. using microphone array as defined in the first part of the talk

Perceptual evaluation [Djordjevic, 2019]

- Headphone-based (binaural) comparison (28 subjects)
- Higher pleasantness ($p < 0.001$) and naturalness ($p < 0.001$) than comparable delay-network based method



Outline

Perceptual-based Reproduction of Plane Waves

Perceptual-based Simulation of Room Acoustics

Conclusions

Perceptual Soundfield Reconstruction

Conclusions

- Physical methods for spatial audio require significant resources
  - Recording and reproduction: many loudspeakers
  - Room Acoustics Simulation: high computational complexity
- Known perceptual effects allow to reduce requirements
  - Recording and reproduction: exploit summing localization effect and small ICTDs to achieve larger sweet spot
  - Room Acoustics Simulation: spend more resources for important perceptual features

Thanks for your attention!
(demos to come)

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(demos to come)

Questions?

Further Reading

Spatial Sound Overview

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Parametrization of ICTD (time-delay microphone array)

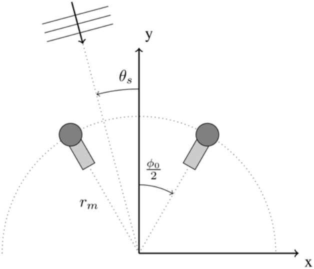
- Convenient now to specify ICTD and ICLD functions of θ_s, including a parameter taking into account how much we rely on ICLD compared to ICLD (time-intensity trade-off)

Parametrization of ICTD (time-delay microphone array)

- Convenient now to specify ICTD and ICLD functions of θ_s, including a parameter taking into account how much we rely on ICLD compared to ICLD (time-intensity trade-off)

- Let the ICTD be defined according to the delay that would be observed on two spatially separated microphones as in figure:

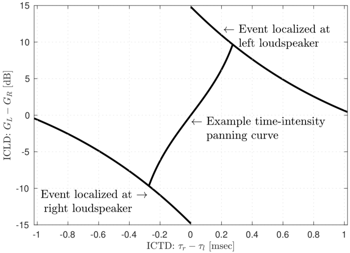
$$\mathrm{ICTD}(\theta_s, r_m) = 2\frac{r_m}{c}\sin\left(\frac{\phi_0}{2}\right)\sin\theta_s$$



where r_m is the array radius

- This parametrization is convenient since it allows to easily extend to the case of recording with circular arrays

Parametrization of ICLDs

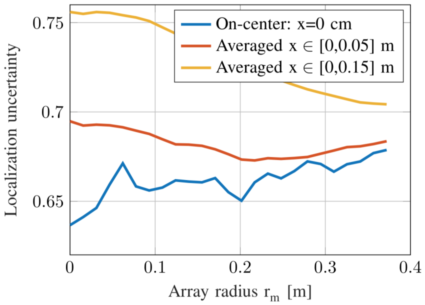


- Psychoacoustic curves give only extreme positions
- Could use different curves, for instance [De Sena et al., 2013]:

$$\mathrm{ICLD}(\theta_s, r_m) = 20\log_{10}\frac{\sin\left(\frac{\phi_0}{2} + \beta(r_m) + \theta_s\right)}{\sin\left(\frac{\phi_0}{2} + \beta(r_m) - \theta_s\right)}$$

  where $\beta(r_m)$ is a parameter used to fit the extrema
- With this parametrization, a higher r_m leads to more reliance on ICTDs and lower ICLDs

Localization uncertainty as a function of array radius



- Larger radii lead to:
  - higher uncertainty for observer in the center
  - lower uncertainty for observer away from the center
- Help reconcile long-stanging debate between academia (preferring intensity methods) and sound engineering community (also using time-intensity methods)

Choosing array radius parameter

- Trade-off between center and off-center
- If we don't know how far the listener will move, then avoid vertical bands mentioned before, which leads to

$$r_m = r_h \frac{\cos\left(\theta_e - \frac{\phi_0}{2}\right) + \frac{\phi_0}{2} + \theta_e - \frac{\pi}{2}}{2\sin^2\left(\frac{\phi_0}{2}\right)}$$

  where θ_e is angle of ear and r_h is head radius
- Interestingly, larger head, means larger array!
- Examples:
  - $\phi_0 = 60^\circ$, $r_h = 9$ cm and $theta_e = 100^\circ$, then $r_m = 0.19$ cm
  - $\phi_0 = \frac{360^\circ}{5} = 72^\circ$, $r_h = 9$ cm and $theta_e = 100^\circ$, then $r_m = 0.16$ cm.

More complex situations

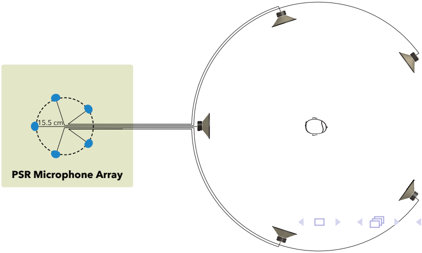
- So far we assumed we know the direction of the plane wave
- Possible approach is to estimate direction of arrival (DOA) and then artificially add ICTD/ICLD
- If multiple incoming waves, can estimated DOAs in time windows (see e.g. Dirac/SDM/SIRR)

Perceptual Soundfield Reconstruction

- Another approach is to connect each microphone with loudspeaker
- Design the microphone directivity pattern to approximate ICLD(θ_s, r_m) [De Sena et al., 2013]
- This makes DOA estimation unnecessary!

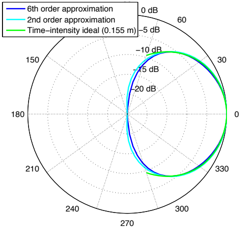
Perceptual Soundfield Reconstruction (PSR) Array

- 5 channels, uniformly distributed, 15.5 cm radius (optimal according to



Microphone directivity that approximates ICLD(θ_s, r_m)

- First-order microphones (e.g. cardioid, hypercardioid) not sufficiently directive for this purpose
- Second-order already sufficient (e.g. differential microphone array [De Sena et al., 2011])



Results of PSR formal listening experiments:

- Comparable performance in the center of the array...
- but larger sweet-spot